

EMShip week, Nantes, February 2015

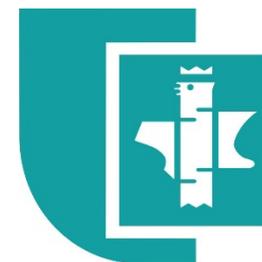


Zachodniopomorski Uniwersytet Technologiczny
w Szczecinie

West Pomeranian University of Technology, Szczecin

Faculty of Maritime Technology and Transport

Department of Ship Structure, Mechanics and Fabrication



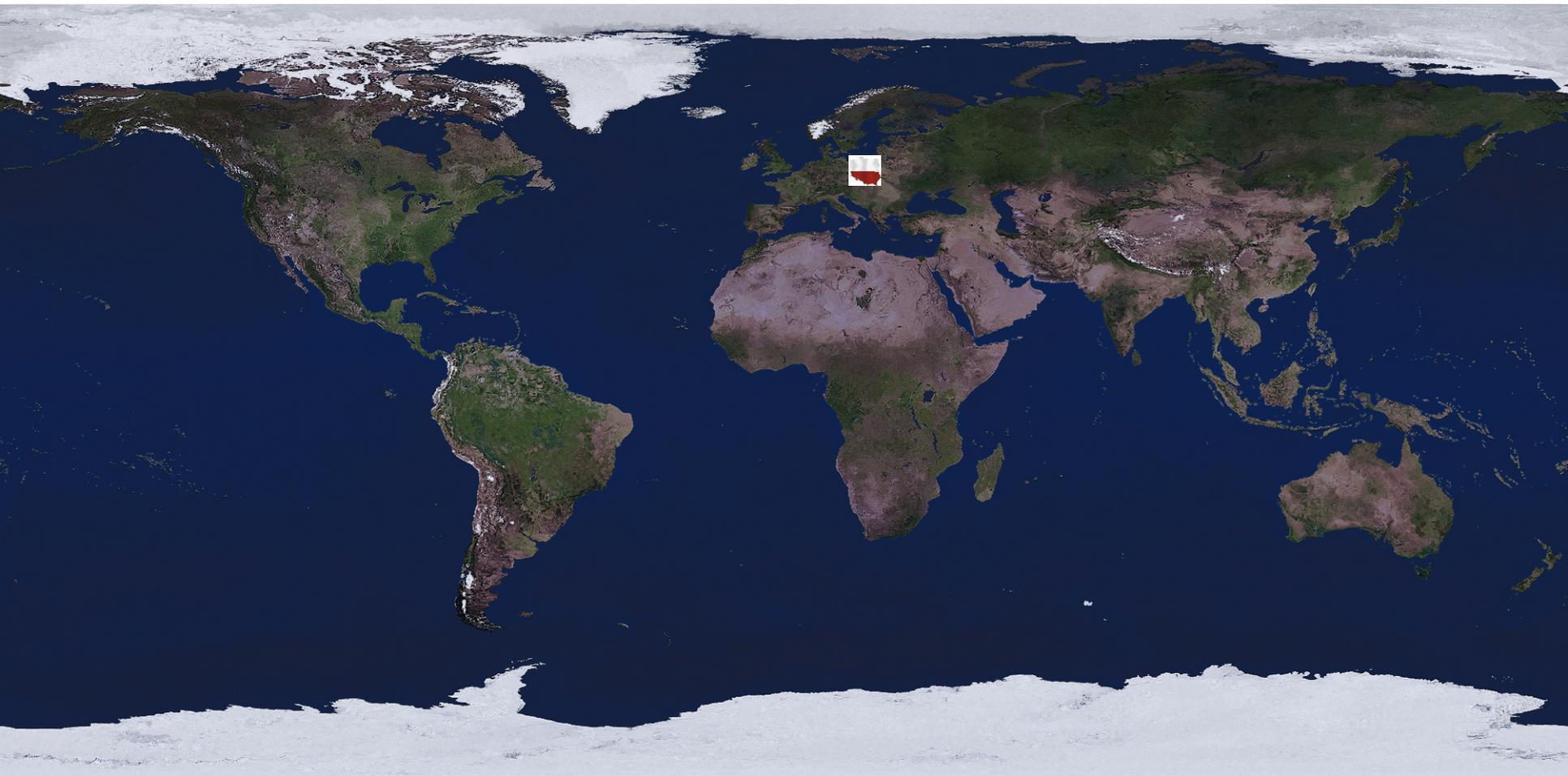
Presentation of various aspects related to the third semester of EMSHIP at ZUT in Szczecin



Prof. Zbigniew Sekulski

EMSHIP Vice Local Coordinator





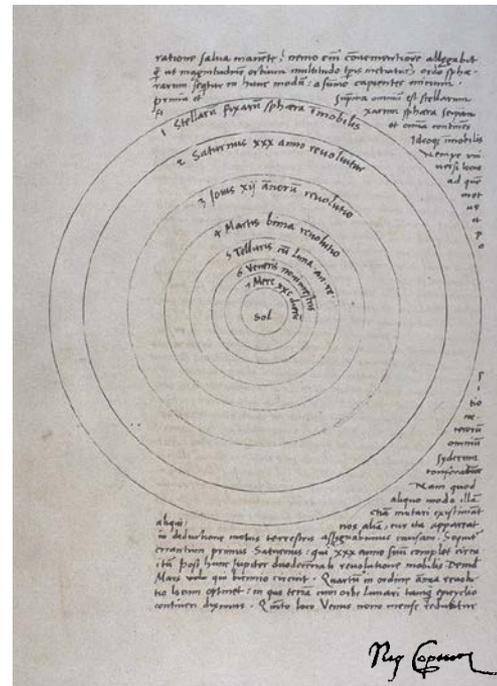
http://nssdc.gsfc.nasa.gov/planetary/image/earth_day.jpg



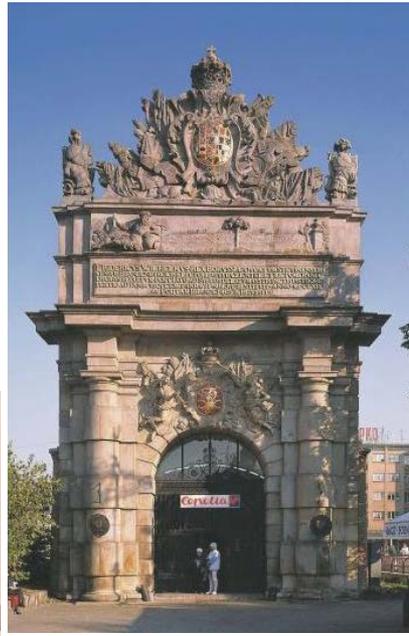
Nicolaus Copernicus (Polish: **Mikołaj Kopernik**) (born in 19 February 1473, died on 24 May 1543) was a Renaissance mathematician and astronomer who formulated a model of the universe that placed the Sun rather than the Earth at its center.

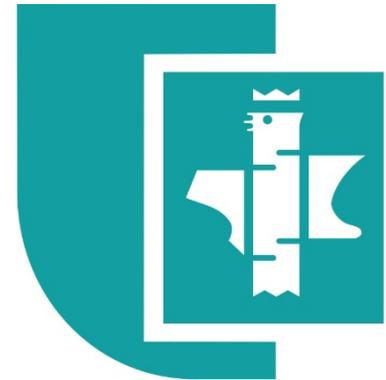


The publication of this model in his book *De revolutionibus orbium coelestium* (*On the Revolutions of the Celestial Spheres*) just before his death in 1543 is considered a major event in the history of science, triggering the Copernican Revolution and making an important contribution to the Scientific Revolution.





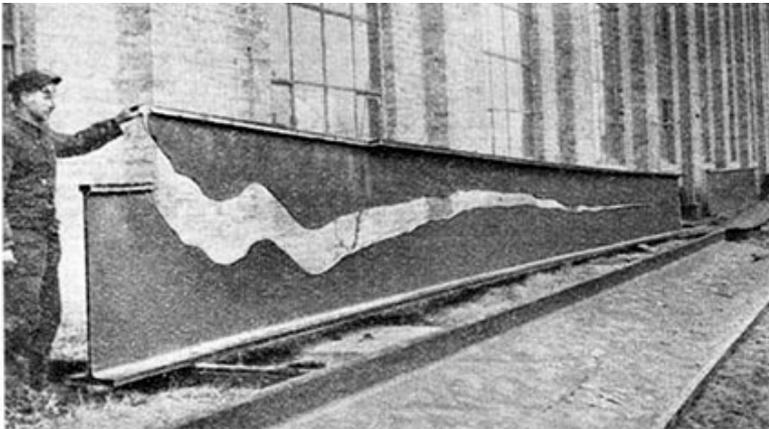
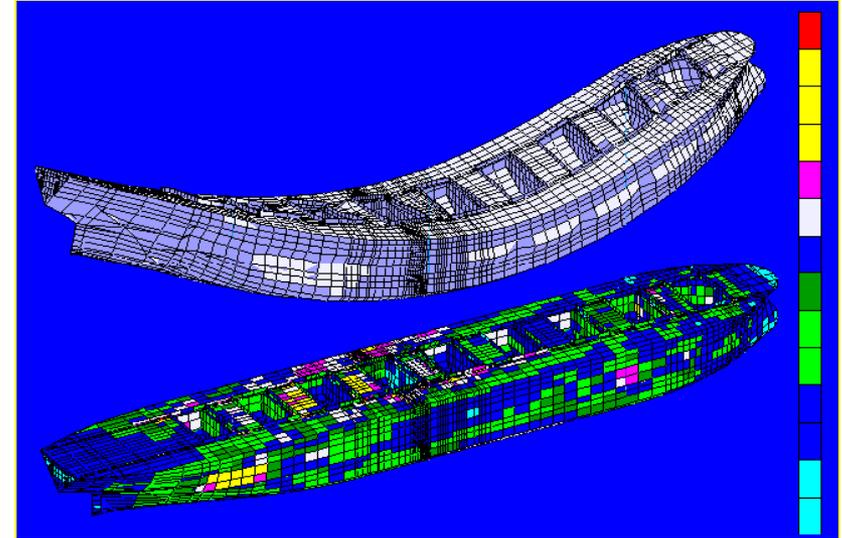




Advanced ship and offshore structural mechanics

Ultimate strength: nonlinear finite element analysis: review of theory and applications to ship structures, FEA guidelines for ship modelling, linear and non linear analysis, static and dynamic analysis; strength of ship structures subject to impact loads.

$$\left[\int_V \rho N_{mq} N_{mp} dV \right] \ddot{d}_q + \left[\int_V D_{kl} B_{lq} B_{kp} dV \right] d_q = \int_A p_m N_{mp} dA + \int_V b_m N_{mp} dV$$



Fatigue and fracture: fundamentals of the fracture mechanics, mechanisms of fatigue failure, methods of fatigue analysis: nominal stress approach, hotspot stress approach, notch stress approach, long-term stress distributions.

$$N \Delta \sigma^m = \frac{1}{C_0 (\sqrt{\pi^m})} \int_{a_0}^{a_f} \frac{da}{(Y \sqrt{a})^m}$$

Advanced ship and offshore structural mechanics

Structural reliability and risk assessment:

Uncertainties, limit state, failure modes, first and second order reliability methods, safety indices, uncertainties in ship structural design, integration of reliability concepts (loads



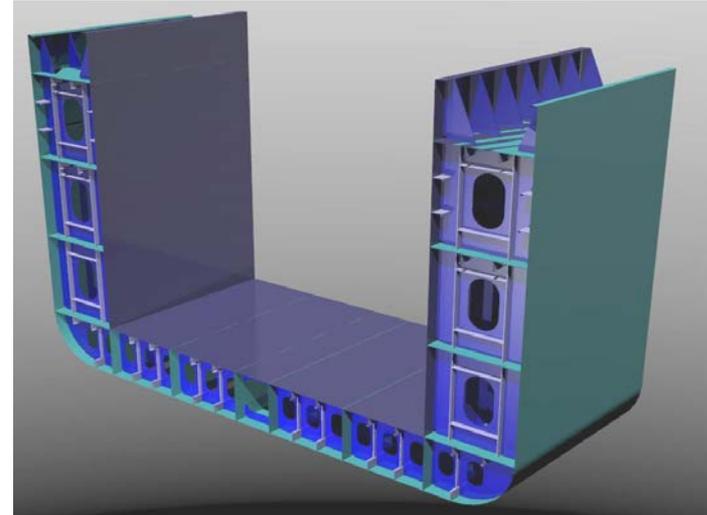
and strength) in calculation of ship structures (rule based approaches and direct calculations).

$$S_1 = \Phi(-\beta) \prod_{j=1}^{n-1} (1 - \beta \kappa_j)^{-0.5}$$

$$S_2 = [\beta \Phi(-\beta) - \varphi(\beta)] \left\{ \prod_{j=1}^{n-1} (1 - \beta \kappa_j)^{-0.5} - \prod_{j=1}^{n-1} [1 - (\beta + 1) \kappa_j]^{-0.5} \right\}$$

$$S_3 = (\beta + 1) [\beta \Phi(-\beta) - \varphi(\beta)] \left\{ \prod_{j=1}^{n-1} (1 - \beta \kappa_j)^{-0.5} - \operatorname{Re} \prod_{j=1}^{n-1} [1 - (\beta + i) \kappa_j]^{-0.5} \right\}$$

Advanced ship and offshore structural design

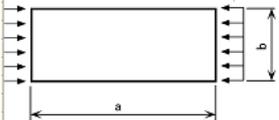


Main characteristics and design objectives of various ship types (passenger ships, bulk-carrier, containership, chemical tanker, liquefied gas tanker, ro-ro, ropax, etc.), use of new materials in the construction of specific ship types (metallic and non-metallic materials, sandwich and core structures), structural arrangement of these specific ship types, loads and strength of these specific ship types, structural details of these specific ship types, IMO conventions and classification societies rules requirements of these specific ship types.

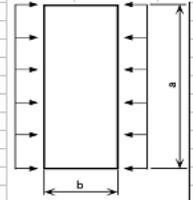
Advanced ship and offshore structural design

Elastic Plate Buckling Under Uni-axial Compression

Longitudinally framed system



Transversely framed system



Green boxes are for data entry!

Calculated on the basis of formulas!

Axial compressive stress σ :	137 MPa	From global hull girder bending
Allowable FOS:	2,5	
Dynamic amplification factor (DAF):	1,00	Include if appropriate
plate thickness $t =$	15,0 mm	$t =$ 15,0 mm
longer side $a =$	2 800 mm	$a =$ 2 800 mm
shorter side $b =$	700 mm	$b =$ 700 mm
$E =$	210 000 MPa	Steel
$\nu =$	0,3	Steel
$\alpha =$	4	
$k (m = 1) =$	18,06	$k (m = 1) =$ 18,06
$k (m = 2) =$	6,25	
$k (m = 3) =$	4,34	
$k (m = 4) =$	4,00	
$K =$	4,00	
$\sigma_{cr} =$	348,26 MPa	$\sigma_{cr} =$ 98,29 MPa

Actual FOS	2,5	OK?	OK
Actual FOS	0,7	OK?	FAIL

plate thickness $t =$	15,0 mm	$t =$ 15,0 mm
longer side $a =$	2 800 mm	$a =$ 2 800 mm
shorter side $b =$	700 mm	$b =$ 700 mm
$E =$	70 000 MPa	Aluminium alloy
$\nu =$	0,33	Aluminium alloy
$\alpha =$	4	
$k (m = 1) =$	18,06	$k (m = 1) =$ 18,06
$k (m = 2) =$	6,25	
$k (m = 3) =$	4,34	
$k (m = 4) =$	4,00	
$K =$	4,00	
$\sigma_{cr} =$	118,55 MPa	$\sigma_{cr} =$ 33,46 MPa

Actual FOS	0,9	OK?	FAIL
Actual FOS	0,2	OK?	FAIL

Global Hull Girder Section Modulus, bending Stress and Factor of Safety (FOS) calculation

The values of bending moment, moment of inertia and section modulus corresponds to Peak Rules of SACS, valid for the calculation and construction of new ship class (RINA, 2014, August).

Green boxes are for data entry!
Calculated on the basis of formulas!

St. Unit (mm, N, Pa)
Breadth (BL) to the bottom
Height of deck, H
Length of the hull, L
Length between perpendiculars, L_{pp}
 C_{σ}
Wave coefficient, C_w
Flexural material density, ρ
Deck structural material density, ρ_{deck}
Flexural material yield, $\sigma_{y,flex}$
Deck material yield, $\sigma_{y,deck}$
Deck material yield, $\sigma_{y,deck}$
Flexural material yield, $\sigma_{y,flex}$
Material FOS
Material allowable
Dynamic amplification factor (DAF)

Material allowable: Material factor α :

94	1,50
120	1,20
142	1,30
150	1,47

Include if appropriate

Plating (Major components one-half of ship hull)

Component	# elements	Area (m²)	Weight (kg)	Worm	Thickness (mm)	Radius (mm)	Total Area (m²)	Height (m)	# Ribbons (m p.p.)	2nd Moment (m⁴ p.p.)	Local Moment (m³ p.p.)	Moment of inertia (m⁴)
Outer bottom plate	1	167,4	1000	0,00	12,0	0,00	167,4	0,00	0,00	0,00	0,00	114 002 000
Inner bottom plate	1	106,7	660	0,00	14,0	0,00	106,7	1,30	112 000	11 200 000	160	65 900 000
Bottom corner girder	4	45,2	276	0,00	9,0	0,00	45,2	0,00	2 000	150 000	50 000	5 100 000
Bottom side girder	2	90,6	552	0,00	12,0	0,00	90,6	0,00	12 000	600 000	200 000	20 700 000
Side plate	1	150,9	943	0,00	10,0	0,00	150,9	4,50	507 000	255 150 000	51 420 000	65 957 072
Inner transverse plate	1	120,0	750	0,00	10,0	0,00	120,0	0,00	115 000 000	150 200	150 200	41 310 000
Main deck plate	1	106,7	660	0,00	14,0	0,00	106,7	0,00	370 000	340 200 000	69	130 447 000
Main deck stringer	1	20,0	125	0,00	10,0	0,00	20,0	0,00	14 000	129 000 000	34	43 004 100
Main deck girder	1	120,0	750	0,00	10,0	0,00	120,0	0,00	70 000	61 250 000	16 607	22 684 405
Main deck plate	1	20,0	125	0,00	10,0	0,00	20,0	0,00	60 000	57 000 000	17	20 580 070
Main deck girder	1	20,0	125	0,00	10,0	0,00	20,0	0,00	252 000	160 000 000	137	27 524 140
Main deck plate	1	120,0	750	0,00	10,0	0,00	120,0	0,00	42 000	22 050 000	16 607	2 075 457
Main deck girder	1	20,0	125	0,00	10,0	0,00	20,0	0,00	40 000	20 000 000	17	1 976 955
Sum		3 260					3 260		1 924 000	1 207 200 000	51 967 200	265 284 745 824

Deck Plating (one-half of ship hull)

Component	# elements	Area (m²)	Weight (kg)	Worm	Thickness (mm)	Radius (mm)	Total Area (m²)	Height (m)	# Ribbons (m p.p.)	2nd Moment (m⁴ p.p.)	Local Moment (m³ p.p.)	Moment of inertia (m⁴)
Deck	1	106,7	660	0,00	14,0	0,00	106,7	0,00	0,00	0,00	0,00	20 000 110
Sum		106,7					106,7		0,00	0,00	0,00	20 000 110

Longitudinals (Minor components one-half of ship hull)

Component	# elements	Area (m²)	Weight (kg)	Worm	Thickness (mm)	Radius (mm)	Total Area (m²)	Height (m)	# Ribbons (m p.p.)	2nd Moment (m⁴ p.p.)	Local Moment (m³ p.p.)	Moment of inertia (m⁴)
Outer bottom longitudinal	1	35,5	219	0,00	10,0	0,00	35,5	0,00	0,00	0,00	0,00	0,000 411
Inner bottom longitudinal	1	35,5	219	0,00	10,0	0,00	35,5	0,00	0,00	0,00	0,00	0,000 570
Main deck longitudinal	1	35,5	219	0,00	10,0	0,00	35,5	0,00	42 070	38 191 072	1 024	14 414 367
Sum		106,5					106,5		42 070	38 191 072	1 024	14 414 367
Total sum		3 366					3 366		1 966 070	1 246 391 070	52 990 610	618 710 146

Half-Ship Values

I_{xx}	343 cm⁴
I_{yy}	1 290 444 905 cm⁴
$A \times h^2$	679 734 637 cm⁴
$I_{xx} + I_{yy}$	618 710 146 cm⁴
5% of $I_{xx} + I_{yy}$	30 935 507 cm⁴

From the goal is as close to 50% as is practical

Full-Ship Values

Area	11 076 cm²
I_{xx}	1 237 420 296 cm⁴
I_{yy}	2 220 244 cm⁴
I_{zz}	3 610 941 cm⁴
Distributed structural mass	4,31 t
Total hull structural mass	527,49 t
Distributed structural weight	42,95 kN
Total hull structural weight	5 270,07 kN
Distributed structural moment	0,00 Nm
Total hull structural moment	0,00 Nm
Sillwater bending Moment in hogging	200 776 100 Nm
Sillwater bending Moment in sagging	273 930 244 Nm
Vertical Wave Bending Moment in hogging	220 776 100 Nm
Vertical Wave Bending Moment in sagging	216 611 732 Nm

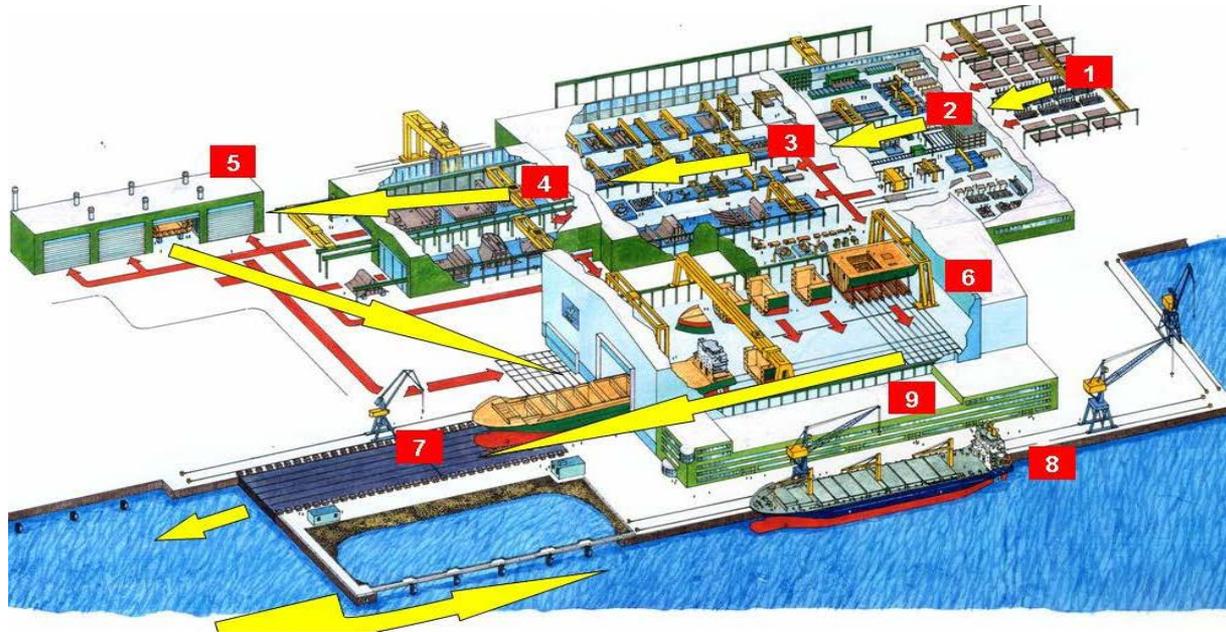
Sillwater deck stress in hogging	90 MPa	2,6	OK
Sillwater deck stress in sagging	122 MPa	3,6	FAIL
Sillwater bottom stress in hogging	56 MPa	1,6	OK
Sillwater bottom stress in sagging	70 MPa	2,1	OK
Hogging deck stress	142 MPa	4,2	FAIL
Hogging bottom stress	80 MPa	2,4	OK
Sagging deck stress	152 MPa	4,5	FAIL
Sagging bottom stress	94 MPa	2,8	FAIL

1 Pa = 1 bar

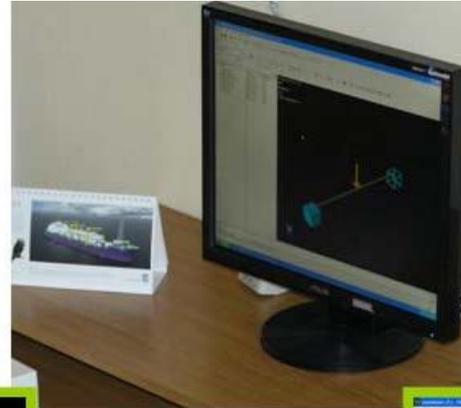
10% Factor of Safety (FOS)	1,2	FAIL
15% Factor of Safety (FOS)	1,5	FAIL
20% Factor of Safety (FOS)	2,0	OK
25% Factor of Safety (FOS)	2,5	OK
30% Factor of Safety (FOS)	3,0	OK
35% Factor of Safety (FOS)	3,5	OK
40% Factor of Safety (FOS)	4,0	OK
45% Factor of Safety (FOS)	4,5	OK
50% Factor of Safety (FOS)	5,0	OK



Advanced ship and offshore production technology

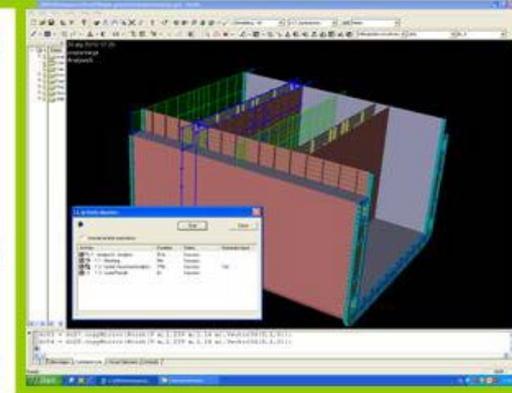
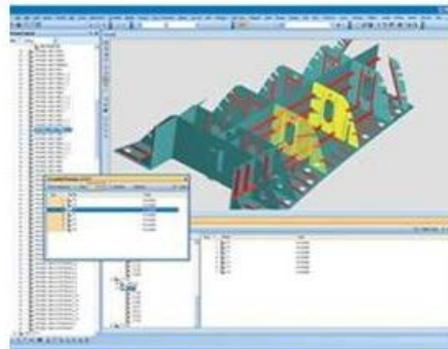
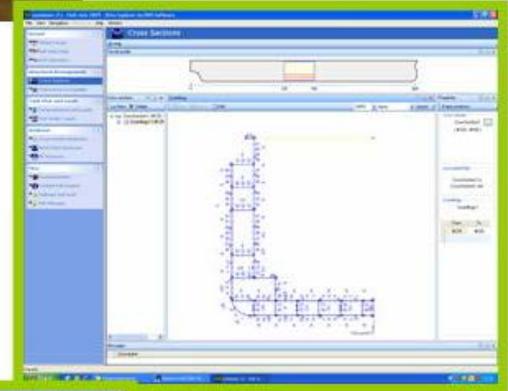
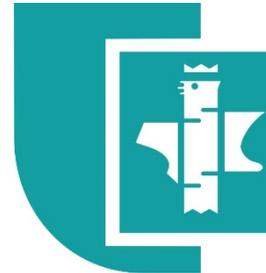
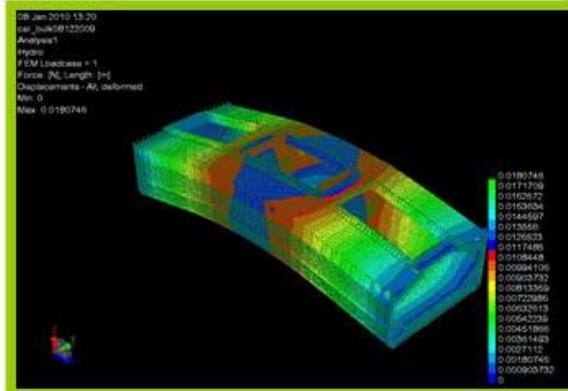


Technology of building of specific ship types, technology of building ships supporting offshore industry, technology of building offshore floating steel and concrete structures, application and manufacturing technology using innovative sandwich structures to ship hull, non-conventional methods of ship launching, underwater technology – fabrication and application of manned and unmanned vehicles.



- ANSYS
- DNV Software:

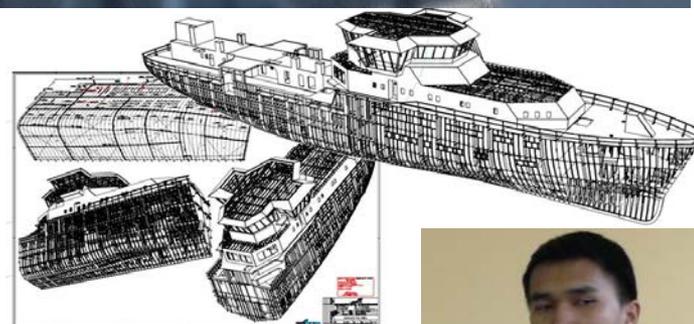
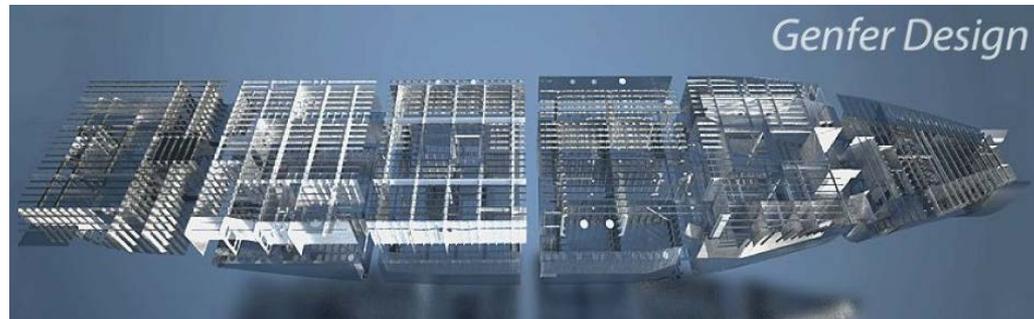
- GeniE
- PreFEM
- Sesam
- Sestra
- WaveShip
- Nauticus Hull
- Poseidon
- Aveva (Tribon)





Andrey Smolko

Structural response of the ship hull elements subject to excitation generated by the main engine



Structural Design of Helicopter Landing Platform on Offshore Ship



Wai Lin Tun

Calculation of Fuel Consumption and Exhaust Emissions from Ship in Ice Conditions



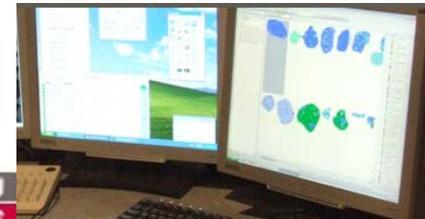
Duong Quang Tan



Jiawei Zou



Investigation of the hull-superstructure interaction in order to predict the contribution of superstructures to hull girder strength





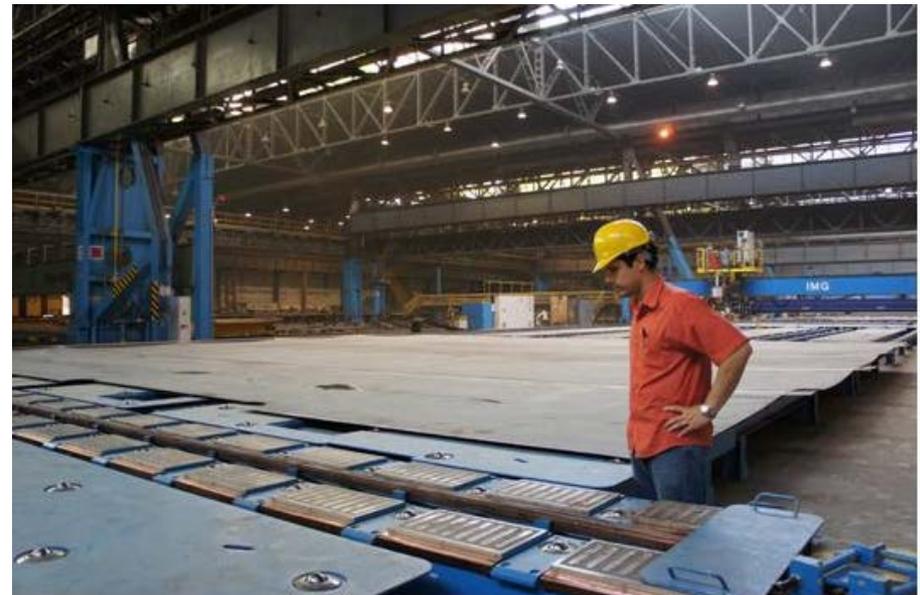
Structural design of Platform Supply Vessel less than 90m



Hailemariam Desalegn Eltiro

Analysis and prediction of welding deformations of ship panels in prefabrication process

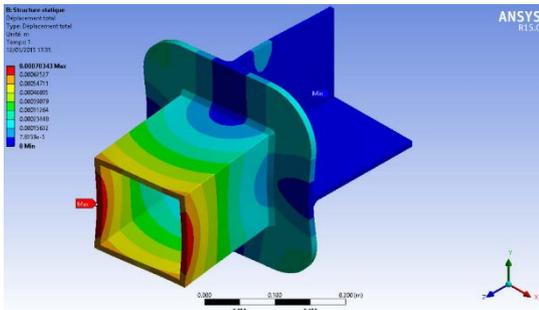
Huggo S. Batista



stx France

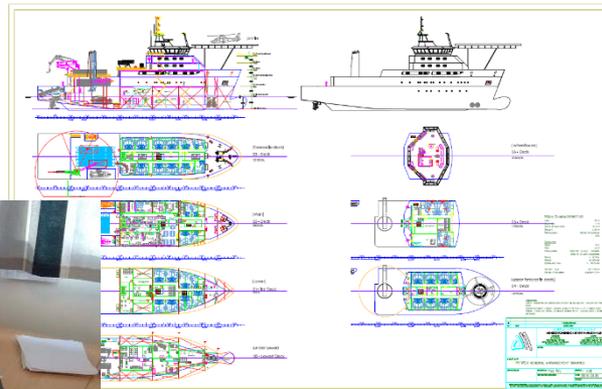
Arnaud Le Pivain

Pillars definition and dimensioning,
Verification and Validation of FEM
parametric model



Yue Wu

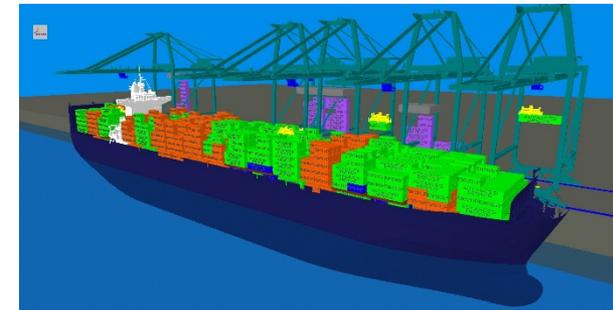
Concept Design of a Station Keeping
Vessel Dedicated to Maintenance of
the Far Shore Wind Farm



UNIVERSIDADE FEDERAL
DO RIO DE JANEIRO

Rasih Onur Suzen

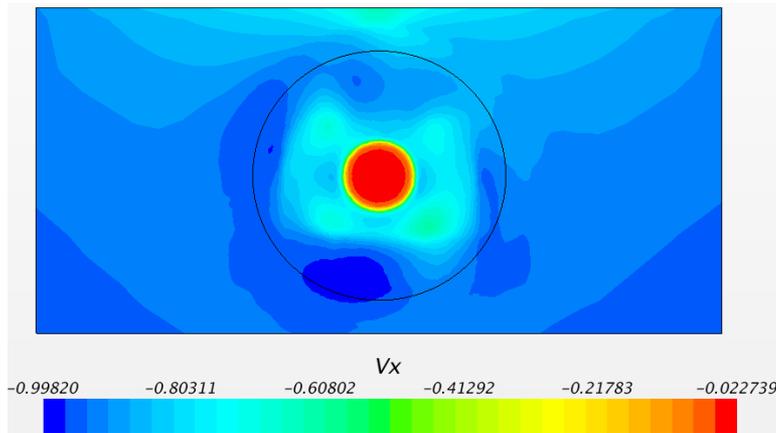
Discrete Event
Simulation Helps to
Improve Terminal
Productivity for New
Design Container Ships





Prabu Duplex

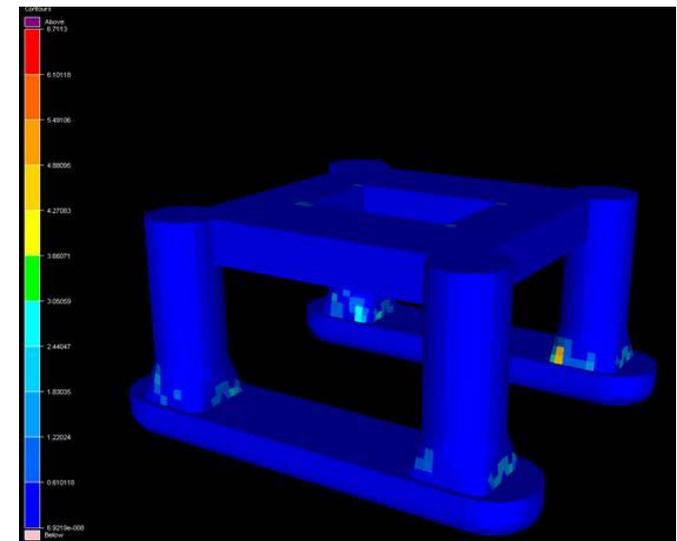
Novel application of large area propeller to optimize Energy Efficiency Design Index (EEDI) of ships



DNV-GL

Md Rezaul Karim

Fatigue Analysis of Offshore Drilling Unit



DNV-GL Group, Gdynia:

- Fatigue calculations analysis of floating drilling platform.



DNV-GL

Crist Shipyard, Gdynia:

- Analysis of manufacturing process with respect to automation and mechanization of welding of ship structures.



Finomar Shipyard, Szczecin:

- Technology of ship hull building.

Marine Repair Yard GRYFIA:

- Analysis of structural strength of floating dock,
- Structural design of icebreakers – modifications.



Ship Research Centre, Gdańsk:

- Thermal/fatigue finite element analysis of structural strength of ship hull elements,
- Experimental investigation of hydrodynamic properties of ships.



Groot Ship Design Poland, Szczecin:

- An investigation into damaged ship stability.

Westcon Design Poland, Szczecin:

- Structural design of a PSV.



Marine Teknikk, Szczecin:

- Structural safety analysis of tankers/containers/bulk carriers/offshore oil rigs in a view of accidents.



Interocean-metal Joint Organization, Szczecin:

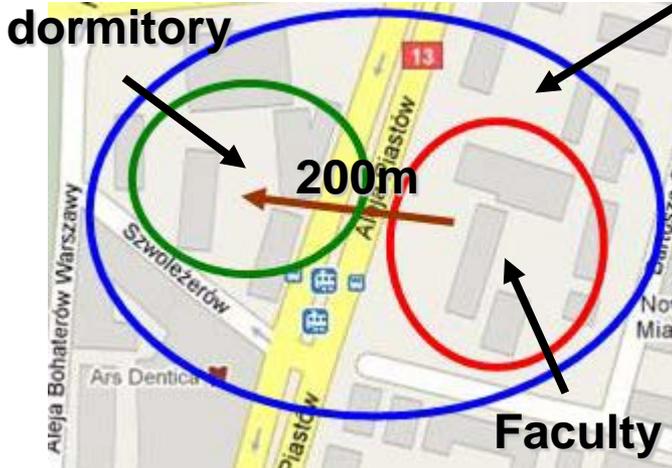
- Preliminary and structural design of a mining ship.

Internships abroad are possible!

Not only in Poland!



http://nssdc.gsfc.nasa.gov/planetary/image/earth_day.jpg





Single room – 490 PLN (120 €) / month



Lunch : 10 – 20 PLN (2.5 – 5 €)



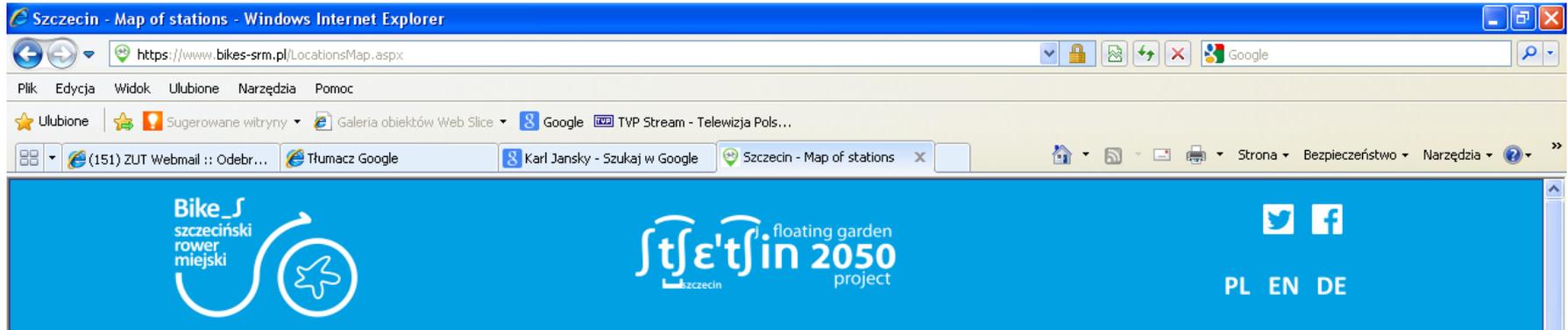
Entrance ticket: 10 – 50 PLN (2.5 – 12 €)



1 € ≈ 4,20
PLN



A beer: 3 – 6 PLN (0.75 – 1.5 €)

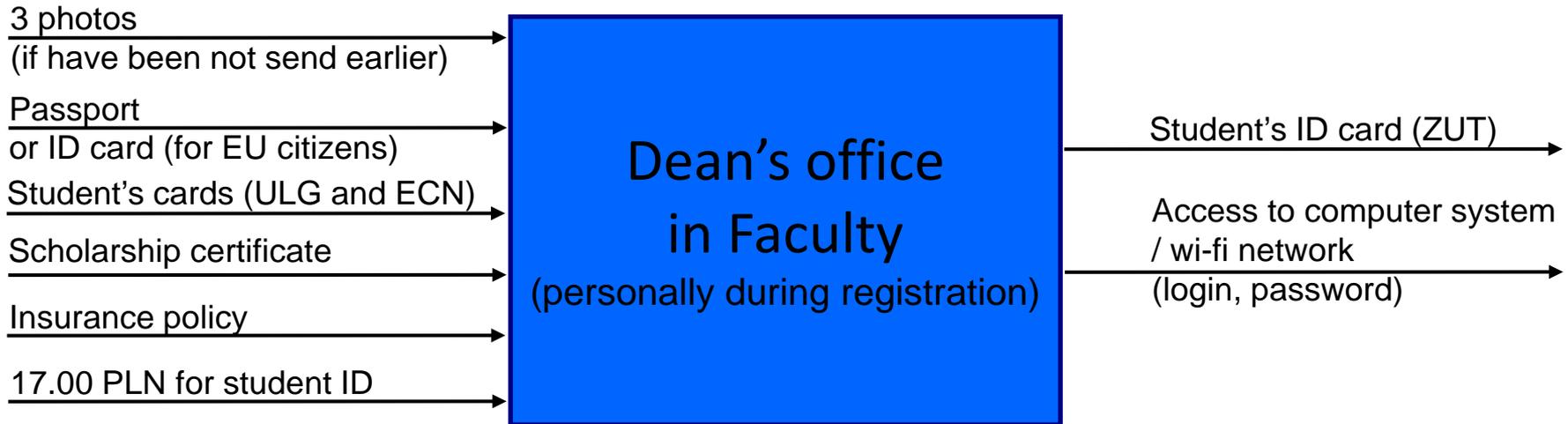
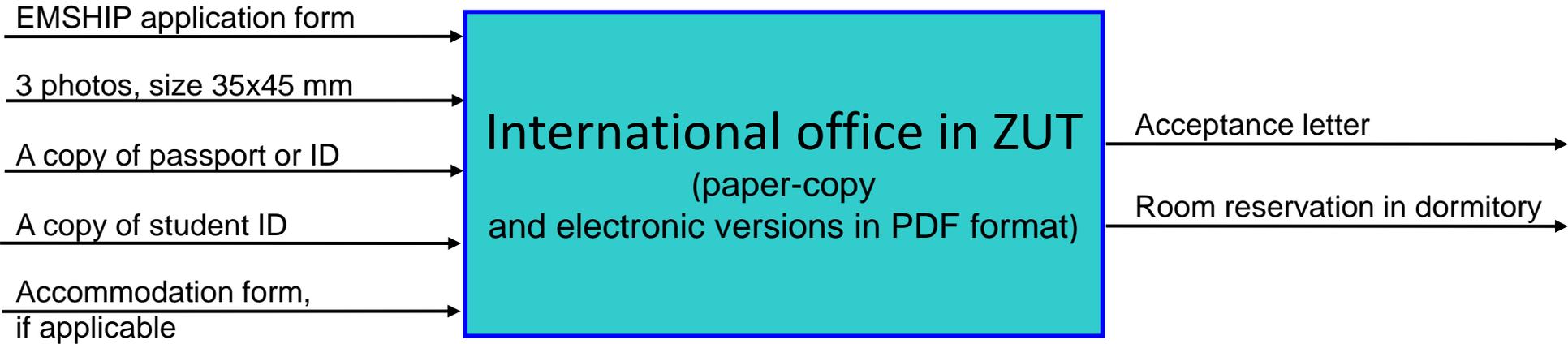


Initial fee: 20 zł
Minimal fee: 10 zł

From 0 to the 20th minute: 0 zł
From the 21th to the 60th minute: 1 zł
From the 61th to 120th minute: 3 zł
From the 121th to the 180th minute: 5 zł
Each subsequent hour: 7 zł

<https://www.bikes-srm.pl>





Why not coming to Szczecin ???



シュチェチン

ꦱꦶꦛꦺꦴꦫꦶꦠꦺꦤ꧀

स्चेचिन

Stettin
Щецин
Estetino
شتاتشين
Στετίνο
ᠰᠢᠴᠡᠴᠢᠨ ᠴᠡᠰᠢ
什切青

